

FEBRUARY 1, 1918

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The Air Patrol

VOLUME IV
Number 1

SPECIAL FEATURES

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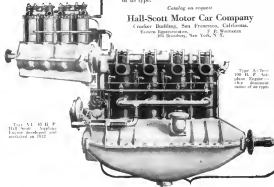
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Vol. IV

February 1, 1918

No. 1

The Design of Air Turbines

By Alexander Klein and Edward P. Warner

While air turbines have occasionally been used to pump gasoline from the tank to an auxiliary, when it could feed by gravity, they were almost for such purposes partly by a matter of cost and error, and our turbine design did not really become important enough to warrant an attempt to establish a scientific principle until the greatly extended use at

the present time, during the last few years, has made absolutely necessary the provision of satisfactory means, in dependent of the engine, for generating considerable quantities of electrical power.

There are three methods of treating the design of air turbines, only two of which will be considered here. First, it may be based as represented, considered by laws of geometrical mechanics, which we shall discuss somewhat later. Second, it may be based on mechanical theory. This is a little used case for any purpose, the student will work on the subject as one out of practical difficulty to obtain, and we shall make an attempt at a treatment of it in this place. The third method, and the one which, in the opinion of the authors, gives by far the most satisfactory results, involves an application of the D'Alembert, or Lagrange, theory of perfect design.

We shall now proceed to a discussion of the methods of designing air turbines in accordance with propeller theory, with occasional mention of the chief modifying factors, the effect of which is so far understood, and shall then enter through the design of a representative fan. Methods of construction will also be taken up.

If we draw a section through the blade at any point, it is apparent that the motion of that section is the resultant of two well-defined components. One of these is parallel to the fan axis, and is equal to V , the speed of translation, while the other is perpendicular to this axis and is equal to three. We may then write this as $\frac{3V}{\gamma}$, where A is the angle between

the resultant motion and the axis of the fan. Since V and $\frac{3V}{\gamma}$

are the same for all portions of the blade, we see that A decreases as r increases.

We may now treat each infinitesimal element of the blade as a wing section, and calculate the forces accordingly. In order to secure forces of the magnitude which may prove to be desirable, each blade element is set at an angle β with the line of resultant motion of the element. (See Fig. 2.)

The forces of a wing section, taken as a wing section, are primarily represented by two graphs, giving, respectively, the force sufficiently parallel and perpendicular to the wind direction. In applying such results to air turbine work, we desire to re-examine these forces with components parallel and perpendicular to the axis, the first being the thrust on the bearings and the "efficiency" or "momentum," which must be overcome by the propeller of the airplane, the second being the force due to the given element available for driving a generator.

Fig. 2 shows the axes in question, L and D being the forces on the element, expressed in the conventional laboratory manner, T and Q those obtained by re-considering.

It is immediately evident that:

$$T = L \cos \beta + D \sin \beta \quad (1)$$

$$Q = L \sin \beta - D \cos \beta \quad (2)$$

$$\text{Torque} = QR = (L \cos \beta - D \sin \beta)r \quad (3)$$

$$\text{Let } \tan \gamma = \frac{L}{D}$$

$$\text{Then } \tan \gamma = \frac{D}{\sqrt{L^2 + D^2}}$$

$$\cos \gamma = \frac{L}{\sqrt{L^2 + D^2}}$$

Simplifying (1), we have $T = \sqrt{L^2 + D^2} (\cos \gamma \cos \beta + \sin \gamma \sin \beta)$
 $\cos \beta = \sqrt{D^2 + L^2} \cos \gamma \cos \beta + \sin \gamma \sin \beta = L \times \frac{\cos \gamma \cos \beta}{\sqrt{L^2 + D^2}}$

Let γ differ from β by less than $1/2$ per cent over the larger portion of the blade, and we may, therefore, write, without serious error $T = L \cos \gamma (A + \gamma)$

(3), similarly, reduce to $Torque = \sqrt{L^2 + D^2} \times c \sin \gamma$ on $A = \frac{1}{2} \pi \gamma$ or A . Ignoring, as before, the small quantity $\sqrt{L^2 + D^2} - L$, we have $Torque = L \times c \times \cos(A + \gamma)$

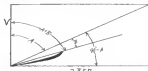


Fig. 2

The useful work done by the element is then: $P = 2\pi r Q = 2\pi r Q \cos(A + \gamma)$, and the power which must be furnished at the surface propeller to overcome its resistance is: $R \times V \times L \times \sin(A + \gamma)$. The efficiency of the element is then:

$$\frac{P}{R \times V \times L \times \sin(A + \gamma)} = \frac{\cos(A + \gamma)}{\sin(A + \gamma)}$$

Station No.	Rad. (in.)	Area	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$
1	1.0	0.0000	0.0000	0.0000
2	1.0	0.0000	0.0000	0.0000
3	1.0	0.0000	0.0000	0.0000
4	1.0	0.0000	0.0000	0.0000
5	1.0	0.0000	0.0000	0.0000
6	1.0	0.0000	0.0000	0.0000
7	1.0	0.0000	0.0000	0.0000
8	1.0	0.0000	0.0000	0.0000
9	1.0	0.0000	0.0000	0.0000
10	1.0	0.0000	0.0000	0.0000

In attacking the actual design of an air turbine, we first decide on a diameter and blade form to be employed. Considerably latitude in these points is permissible, and it is generally possible, after a little experience, to guess them closely enough at the first trial. Several stations, from flow to right is usual, are then placed at approximately equal intervals along the blade, and the section to be used at each is selected. These

Station No.	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000

sections should be of such a nature as to give at least a fairly high L/D , and should, possible, meet other in general outline, although becoming thicker as the hub is approached.

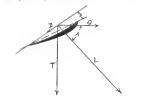


Fig. 3

The left per running face and the efficiency at each station are then determined, the left being $A \times D \times F$, where A is the lift coefficient from a laboratory test, D the width of blade, and F

the resultant velocity through the air, F' being equal to $F \times \cos(\gamma)$. Having L , the torque and thrust per running foot of each must now be determined from the expression: $L \times r \times \cos(A + \gamma)$ and $L \times \sin(A + \gamma)$.

The next step is to plot a torque curve and thrust curve, the abscissa of these curves representing the radial distance from the propeller axis to the station, that calculates the torque and thrust per running foot, respectively. The areas under these curves then represent the torque and thrust for the entire blade, and through the data for computing the power developed and the resistance opposed by the turbine to the advance of the turbine.

Where the power required is commonly known in advance, it is customary to write the blade width at each station as a function of L , an unknown. We can then, after the simplification of the graphical integrations of the curves, solve for a value of L which will give exactly the necessary torque, thereby making an application of cut-and-try methods.

As alternative method of procedure is to draw curves of torque and thrust, the latter quantity being readily convertible into thrust.

Having given, in brief explanation of the method, we shall commence the design of an actual air turbine. The assumed conditions are a speed of translation of 60 m.p.h., a rotary speed of 2000 r.p.m., and a required power of 900 watts. We shall try, as an initial line, a 10 in. diameter. A table may then be drawn up as follows:

Station No.	Rad. (in.)	Area	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$
1	1.0	0.0000	0.0000	0.0000
2	1.0	0.0000	0.0000	0.0000
3	1.0	0.0000	0.0000	0.0000
4	1.0	0.0000	0.0000	0.0000
5	1.0	0.0000	0.0000	0.0000
6	1.0	0.0000	0.0000	0.0000
7	1.0	0.0000	0.0000	0.0000
8	1.0	0.0000	0.0000	0.0000
9	1.0	0.0000	0.0000	0.0000
10	1.0	0.0000	0.0000	0.0000

We shall now build the propeller sections Nos. 3, 6, 8, 9, 10 and 11 for the four elements. These sections, due to the smaller size number of the lower face, give a large lift coefficient, thereby making it easy to secure the required power with the relatively small diameter proposed. From the experimental data given for these sections, we find L/D and C_L as F' , we tabulate our table as below:

Station No.	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$	$\frac{P}{R \times V \times L \times \sin(A + \gamma)}$
1	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000
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7	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000

L , Q and F' in the above, are expressed in lbs. (or lbs. ft.) per running ft. of blade, and k is the maximum blade width in in.

We now plot curves of Q and F' in Fig. 4. The former only

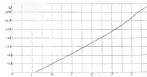


Fig. 4

is shown to avoid confusion. The area under the Q curve is found to be 43.2 square inches, corresponding to a torque of 216 ft. lbs. $\frac{1}{2}$ of the area under the F' curve corresponds to a thrust of 1.00 lb.

It is desired to generate, as previously specified, 900 watts, and this is equal to 900 ft. lbs. per sec. Then, 216×900

and $Q = 1.812$ lbs. ft., we being 60 revs. per sec. Doubling the area due to the number of blades, we see that the torque due to each blade must be 432 ft. lbs. Since the graphical integration just performed shows us that this torque is equal to 216 ft. lbs. ft., we may equate the two expressions, and k is then 1.35 in. The width of each blade element may then be obtained by substituting this value for k in the volume of the design computations.

Substituting k in the expression for thrust, and multiplying by the number of blades, we find that the presence of 16 air surfaces adds 7.9 lbs. to the total load resistance of the air turbine. The work done in driving it through the air is then equal to the resistance times the speed, or 708 ft. lbs. per sec., and the efficiency is 84 per cent.

Now, however, the power driving the turbine should meet

almost impossible to say anything definite about the effects of interference due to elements in or behind the fan. Since the effect of the blade elements is to create a partial vacuum above their upper surfaces (i.e., behind the turbine), while the effect of any body placed in a wind, and especially a body set of low resistance form, is to "back up" the air (i.e., front) of it,

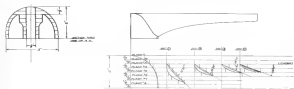
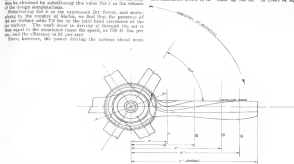


Fig. 6

but be transmitted through the propeller, and since the efficiency of the propeller is likely to be about 75 per cent, the total efficiency of the air turbine as a generating device is small in the present of these two quantities, or, roughly, 60 per cent. Although this appears rather low, the power developed is so small in comparison with the total power of the turbine that the slight loss is more than compensated for by saving the generator function at all times, whether or not the engine is running, and by the avoidance of additional losses given driven by the windblast.

A drawing of this turbine is given in Fig. 5, and a photograph in Fig. 1. The sections and sections are shown in the same way as for an air propeller, although less care is needed in its propeller design, and it will not be necessary to break the surface of layers.

Until the performance of further experimental work, it is

creating a positive pressure, it is evident that these two tendencies will oppose each other, and that there will be some loss of power and efficiency as a result, but a quantitative determination of these losses by analytical methods would be a long time.

The nature of the flow about the blades of an air turbine has not been fully determined. Some work is done by the system, energy must be withdrawn from the air, and it is probable that there is a certain dissipation of speed of the air approaching the turbine before it actually impinges on the blades.

If it is desired to find the work done and efficiency under other conditions, when the speed of rotation, or the speed of advance, or both, are varied, the procedure is that already described, save that the angle $(A + \gamma)$ has now been fixed, and



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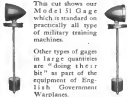
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